Abstract: The generated torque ripples from the BLDC motor is the main issue that affects the drive performance of the BLDC drive system. In this concept, a new switching technique to minimize the torque ripples due to current commutation is proposed. The presented scheme has been implemented using a commercial and low-cost mid-range PIC microcontroller to generate the modified pulse width modulation (PWM) control signals. An analysis of phase current during commutation time is carried out. Simulation results verify the effectiveness of proposed method. Results had shown a smoother output torque and current produced in comparison with that using conventional PWM control technique with an average of 50 % reduction in the generated torque ripples. Brushless DC (BLDC) motor has a permanent magnet rotor and a wound field stator, which is connected to a power electronic switching circuit. The availability of high energy- density permanent magnet (PM) materials at competitive prices, the commercial availability of low-cost microtome- trolleys and reduction in cost of powerful fast digital signal processors (DSPs) along with the advances in semiconductor-tor power switches have opened up wider area for permanent magnet brushless motor drives to be a competitive solution meeting the market demands due to their control simplicity, low torque per weight ratio and compact construction. The proposed concept can be implemented to Communication Torque Ripple Reduction in Brushless DC Motor using current control technique by using Matlab/Simulink software.

Keywords: BLDC Motor, Modified, SEPIC Converter, Commutation Torque Ripple, Dc Link Voltage Control.

I. INTRODUCTION

Brushless DC Motor (BLDCM), has been widely used in industries that require high reliability and precise control due to its simple structure, high power density and wide speed range [1]. Torque ripple, which occurs during commutation period, has always been one major factor in preventing BLDCM from achieving high performance. Two general approaches have been proposed to reduce the torque ripple. The first approach is to improve the motor’s geometrical structure [2]. The second approach is to control the winding currents to overcome the disturbances [3]. More studies are being done to identify the sources, characteristics and minimization of torque ripple [3]. A new approach to optimize current waveform based on d-q frame, which results in minimum torque ripple and maximum efficiency of BLDC motor drives is proposed in [6]. DTC is applied to BLDC Motor drives to achieve instantaneous torque control and reduced torque ripple is described in [7]. The commutation torque ripple and its compensation technique have been analyzed theoretically in [8]. Researchers introduced some special topology of a circuit to BLDCM drives to control its input voltage in [11]. In, the current slopes of the incoming and outgoing phases in the commutation period are equalized. In [12], a buck converter is used, and commutation torque ripple is greatly reduced at low speed.

In [13], a super lift Luo converter is placed at the front of the inverter to produce desired DC link voltage and the commutation torque ripple is reduced at high speed. Those methods suffer from slow voltage adjustment and can achieve torque pulsation reduction only in low or high speed regions. A new approach of minimizing commutation torque ripple for BLDCM based on Single ended primary inductor converter(SEPIC) is presented in [14]. But the conventional SEPIC has pulsating output current similar to buck boost converters. In addition, the SEPIC converter transfers all its energy via the series capacitor so a capacitor with high capacitance and current handling capability is required. In this project, a Modified SEPIC (MSEPIC) converter is proposed as a step-up and step-down converter having high power conversion efficiency and minimized voltage and current stress than the classical SEPIC topology. The idea of this proposed work is to drive phase currents to increase and decrease in the identical slope, resulting in the reduction of pulsed commutation torque ripple. Simulation results prove that the torque ripple is reduced when compared with the conventional method.

II. COMMUTATION TORQUE RIPPLE IN BLDCM

Ideally, the current drawn by the BLDCM, with trapezoidal back EMF, takes the form of rectangular waveform [8] as shown in Fig.1. This kind of current waveform will produce a constant torque. Practically, the smoothness in torque waveform is not observed and torque ripple is prevalent. Various non – linearity in the machine will result in the disruption of the ideal rectangular current waveform thereby resulting in torque ripple. The excitation
current waveforms do not change instantaneously and a variable commutation time for different speeds is observed [18] as shown in Fig.2.

During this commutation time, Torque ripple occurs due to the difference between the time taken by the ongoing phase ‘b’ current to reach the saturation value and the time taken by the off going phase ‘a’ current decay to zero. In order to eliminate the dip in the Torque waveform, the difference in the commutation time for ongoing and off going phase currents should be made zero [18] as shown in Fig.3. This torque dips can be reduced by suitable dc link voltage control method during the commutation time. This can be achieved by using proposed MSEPIC in B LDCM drives.

III. MODIFIED SEPIC CONVERTER

The circuit topology of the conventional SEPIC Converter [19] is presented in Fig.4. The wide range of input voltages can be realized because of the step-up and step down static gains of SEPIC converter. However, SEPIC converter suffers from higher voltage and current stress [19]. This disadvantage can be eliminated by using the proposed M-SEPIC converter circuit. Here, the modification of the SEPIC converter is accomplished by including diode Dm and capacitor Cm as shown in Fig.5. A multiplier cell (Cm and D) reduces the switch stress in the proposed converter. The capacitor Cm is charged with the output voltage of the classical boost converter. Hence, the voltage applied to the inductor L2 during conduction is higher compared with the classical SEPIC, thereby increasing the static gain.

The continuous conduction- mode (CCM) operation of the MSEPIC converter presents the following two modes.

**Mode 1:** In this mode the switch S is turned off as shown in Fig.6(a) and the energy stored in the input inductor L1 is transferred to the output through the capacitor C1 and output diode Do, and also to the capacitor Cm through the diode Dm. Therefore, the switch voltage is equal to the capacitor Cm voltage. The energy stored in the inductor L2 is transferred to the output through the diode D0.

**Mode 2:** In this mode the switch S is turned-on and the diodes Dm and D0 are blocked as shown in Fig.6(b), and the
inductors $L_1$ and $L_2$ store energy. The input voltage is applied to the input inductor $L_1$ and the voltage $(V_{cs} - V_{cm})$ is applied to the inductor $L_2$. The voltage $V_{cm}$ is higher than the voltage $V_{cs}$. The inductor $L_1$ current is equal to the input current and the inductor $L_2$ current is equal to the output current.

**IV. PROPOSED TORQUE RIPPLE MINIMIZATION TOPOLOGY FOR BLDCM**

A Modified SEPIC Converter with a switch over IGBT for implementing the dc link voltage adjustment is shown in Fig.7. In Fig. 7, $S_1$, $S_2$, $S_3$ are power MOSFETs. By operating $S_1$ appropriately, the energy storage components $L_1$, $L_2$, $C_s$, $C_0$ and $C_m$ of the M-SEPIC can be adjusted to get the desired voltage. $S_2$ and $S_3$ are switched over power MOSFETs used for choosing between the inputs of the inverter $V_s$ and the output voltage of the MSEPIC $V_o$.

**Fig. 7. Configuration of BLDCM driving system with MSEPIC Converter.**

$V_o$ can be calculated as

$$V_o = \frac{1 + D}{1 - D} \times V_s$$  \hspace{1cm} (1)

Where, $D$ is the Duty ratio. $Em$ is proportional to speed, i.e.,

$$Em = K_e \omega$$ \hspace{1cm} (2)

Where $K_e$ is the back EMF co-efficient and $\omega$ is the speed of the machine. Then, the duty ratio of $S_1$ for satisfying $V_o = 4Em$ from [14] can be calculated by

$$D = \frac{4K_e \omega - V_s}{V_s + 4K_e \omega}$$ \hspace{1cm} (3)

According to above equation, the duty ratio of $S_1$ corresponding to the desired dc link voltage can be estimated by measuring the motor speed. The relationship between the duty ratio and speed is shown in Fig.8. The duty ratio calculations are done by assuming the input voltage $V_s$ as 200V. To achieve an immediate change of the input voltage of inverter, $S_2$ and $S_3$ should be complementary to each other. At the beginning of every commutation, $S_2$ is switched OFF and $S_3$ is switched ON. The MSEPIC converter stops adjusting, and the output voltage remains constant. Once commutation is over, $S_2$ is switched ON and $S_3$ is switched OFF. The MSEPIC converter will start regulating again, and its output voltage will reach the expected value before the next commutation. The flowchart for the proposed method is clearly indicated in Fig.9.

**Fig. 8. Duty ratio with respect to speed.**

**Fig. 9. Flowchart of the proposed method for one electrical cycle.**

**IV. INTRODUCTION TO FUZZY LOGIC CONTROLLER**

A new language was developed to describe the fuzzy properties of reality, which are very difficult and sometime even impossible to be described using conventional methods. Fuzzy set theory has been widely used in the control area with some application to dc-to-dc converter system. A simple fuzzy logic control is built up by a group of rules based on the human knowledge of system behavior. Matlab/Simulink simulation model is built to
study the dynamic behavior of dc-to-dc converter and performance of proposed controllers. Furthermore, design of fuzzy logic controller can provide desirable both small signal and large signal dynamic performance at same time, which is not possible with linear control technique. Thus, fuzzy logic controller has been potential ability to improve the robustness of dc-to-dc converters. The basic scheme of a fuzzy logic controller is shown in Fig 10 and consists of four principal components such as: a fuzzy fication interface, which converts input data into suitable linguistic values; a knowledge base, which consists of a data base with the necessary linguistic definitions and the control rule set; a decision-making logic which, simulating a human decision process, infer the fuzzy control action from the knowledge of the control rules and linguistic variable definitions; a de-fuzzification interface which yields non fuzzy control action from an inferred fuzzy control action [10].

Fig.10. General structure of the fuzzy logic controller on closed-loop system.

The fuzzy control systems are based on expert knowledge that converts the human linguistic concepts into an automatic control strategy without any complicated mathematical model [10]. Simulation is performed in buck converter to verify the proposed fuzzy logic controllers as shown in Fig.11.

Fig.11. Block diagram of the Fuzzy Logic Controller (FLC) for dc-dc converters.

**Fuzzy Logic Membership Functions:** The dc-dc converter is a nonlinear function of the duty cycle because of the small signal model and its control method was applied to the control of boost converters. Fuzzy controllers do not require an exact mathematical model. Instead, they are designed based on general knowledge of the plant. Fuzzy controllers are designed to adapt to varying operating points. Fuzzy Logic Controller is designed to control the output of boost dc-dc converter using Mamdani style fuzzy inference system as shown in Figs.12 to 14. Two input variables, error (e) and change of error (de) are used in this fuzzy logic system. The single output variable (u) is duty cycle of PWM output.

**Fig. 12. The Membership Function plots of error.**

**Fig.13. The Membership Function plots of change error**

**Fig.14. the Membership Function plots of duty ratio**

**Fuzzy Logic Rules:** The objective of this dissertation is to control the output voltage of the boost converter. The error and change of error of the output voltage will be the inputs of fuzzy logic controller. These 2 inputs are divided into five groups; NB: Negative Big, NS: Negative Small, ZO: Zero Area, PS: Positive small and PB: Positive Big and its parameter [10]. These fuzzy control rules for error and change of error can be referred in the table that is shown in Table II as per below:

**TABLE II: Table Rules for Error and Change of Error**
V. SIMULATION RESULTS

Simulation results of this paper is as shown in bellow Figs.15 to 23.

Fig.15. Matlab/simulation circuit of conventional for reducing commutation torque ripple in BLDCM drive.

Fig.16. Matlab/simulation circuit of conventional for reducing commutation torque ripple in BLDCM wave form of current and electromagnetic force.

Fig.17. Matlab/simulation circuit of conventional for reducing commutation torque ripple in BLDCM wave form of speed.

Fig.18. Matlab/simulation circuit of conventional for reducing commutation torque ripple in BLDCM wave form of torque.

Fig.19. Matlab/simulation circuit of conventional for SEPIC converter reducing commutation torque ripple in BLDCM drive.

Fig.20 Matlab/simulation circuit of conventional for SEPIC converter reducing commutation torque ripple in BLDCM wave form of current and electromagnetic force.
VI. CONCLUSION

In this project a fuzzy logic topology based on Modified SEPIC converter is analyzed for reducing commutation torque ripple in BLDCM drives. The reduction in voltage and current stress of the main switches are the main advantage of this topology. Simulation is done for wide range of speeds and from the results it is apparent that the torque ripple is effectively reduced. Fuzzy logic implementation of BLDCM drive with conventional control is done using FPGA. The close correlation between simulation results illustrate the relevance of the topology for torque ripple minimization.

VII. REFERENCES

Communication Torque Ripple Reduction in Brushless DC Motor using Modified SEPIC Converter and Current Control Technique